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			A PRODNIEWS DOOKET NUMBER								
FORM PTO-139 (REV 12-29-99)		RTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE	ATTORNEY'S DOCKET NUMBER								
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	DESIGNATED/ELECT	ED OFFICE (DO/EO/US)	U.S. APPLICATION NO. (If known, see 37 CFR 1.5)								
	CONCERNING A FILI	NG UNDER 35 U.S.C. 371	09/601013								
	TIONAL APPLICATION NO.	INTERNATIONAL FILING DATE 17 Feb. 1999	PRIORITY DATE CLAIMED 18 Feb. 1998								
	FINVENTION										
DEV	<u>ICE FOR TESTING T</u> NT(S) FOR DO/EO/US	HE ELECTROMAGNETIC COMPAT	TRILITY OF SYSTEMS HAVING LARGE PIMENSIONS								
WIL	BERTIJAN PAUL		* II-II-II-II-II-II-II-II-II-II-II-II-II-								
Applicant	herewill submits to the United Stat	es Designated/Elected Office (DO/EO/US) the follo	owing items and other information:								
1. 🔀	This is a FIRST submission of iter	ns concerning a filing under 35 U.S.C. 371.	45								
2.		ENT submission of items concerning a filing under									
3. 4. 4.	examination until the expiration of	nal examination procedures (35 U.S.C. 371(f)) at an the applicable time limit set in 35 U.S.C. 371(b) at Preliminary Examination was made by the 19th me	nd PCT Articles 22 and 39(1).								
5. 🔼	A copy of the International App	olication as filed (35 U.S.C. 371(c)(2))									
		(required only if not transmitted by the Intern	national Bureau).								
b. As been transmitted by the International Bureau.											
 c. is not required, as the application was filed in the United States Receiving Office (RO/US). 6. A translation of the International Application into English (35 U.S.C. 371(c)(2)). 											
7.		ne International Application under PCT Article									
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	b. have been transmitted	by the International Bureau.									
	c. have not been made; h	owever, the time limit for making such amend	ments has NOT expired.								
	d. A have not been made ar										
8.		ts to the claims under PCT Article 19 (35 U.S.	C. 371(c)(3)).								
	An oath or declaration of the in	ventor(s) (35 U.S.C. 371(c)(4)).									
10. 🔼	A translation of the annexes to (35 U.S.C. 371(c)(5)).	the International Preliminary Examination Re	port under PCT Article 36								
Items 1	1. to 16. below concern docume	ent(s) or information included:									
11.	An Information Disclosure Stat	ement under 37 CFR 1.97 and 1.98.									
12.	An assignment document for re	cording. A separate cover sheet in compliance	e with 37 CFR 3.28 and 3.31 is included.								
13.	A FIRST preliminary amendme	nt.									
	A SECOND or SUBSEQUENT	preliminary amendment.									
14.	A substitute specification.										
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17. The fol	lowing fees are submitte				CAL	CULATIONS	PTO USE ONLY				
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Processing fee of \$130.00 for furnishing the English translation later than 20 30 months from the earliest claimed priority date (37 CFR 1.492(f)).											
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Device for testing the electromagnetic compatibility of systems having large dimensions

Especially in the military field it is known that EMC-susceptibility tests are based on a pulseshaped short stimulation. With these test by far stronger inhomogeneous fields come to application. Through the usual shape of the wave guides from the source to the termination of the impulse, no optimal testing field for civil requirements can be produced. Bends in the wave guide, geometrical changes of the wave guide from the source to the termination relative to its return conductor, a mismatched adaptation between the measurement of the equipment under test and the testing volume, the arrangement of the loading device in the testing volume and the testing volume loss originating by this, rail shaped and other sparking gaps between impulse source and field-generating wave guide arranged in an angle to the wave guide which differ largely in the geometry from the wave guide, lead to reflections which influence the extension of the pulse negatively and, by this, lead to a deterioration of the produced electromagnetic field in the testing volume. Furthermore, too long wave guides lead to an obliteration of the pulse, respectively a radiation of energy, as usual in many installations, and, with that, restrict its frequency spectra. With sine shaped fed wave guides or strip lines dimension-conditioned frequency range restrictions occur. Also with other similar testing methods, as the use of antennas with a determined directive diagram in an appropriate dimensioned unachoic chamber as usual in the automobile technique, no economical justifiable testing against electromagnetic radiated fields is possible for larger systems. In particular, no special susceptibility test for a whole train is existing at present.

Burst generators, which produce nano second impulses (5/50 ns) in fast succession and over controllable spark gaps with variable amplitudes, belong also to the state of art in the technique (DE 43 40 514 C2). However, conditioned by construction, these burst generators cannot replace a testing device described in the above mentioned patent claim for systems having large dimensions but serve rather the conductor led component test.

The advantages obtained by the invention consist in particular of the enormous time saving in testing time, the obtained field quality and the applicability for any long equipment under test with simultaneous minimal length of a single pulse conducting wave guide achieved through the modular structure. The test of a whole train in the far field, without a movement of the radiation

ART 34 ANDT source while keeping the field homogeneity, can be conducted with a wave guide width differing only little from the train width.

> The invention mentioned in the patent claim underlies the problem, to create generally for a complete system having large dimensions, a homogeneous testing field accepted by rules of the civil EMC-susceptibility-technique (ENV 50140).

> This problem will be solved by the characteristics mentioned in patent claim 1 that several of these IGW, ICW, return conductors and terminating characteristic impedance's in the described arrangement combine units parallel, modular, to a common triggering mechanism and, by this, creating a testing chamber applicable for a system with large dimensions.

> The advantages obtained by the invention consist especially in, instead of the piecewise EMCsusceptibility-test of systems with large dimensions leading to wrong results, a complete illumination of the equipment under test can be made (all) at once in nano seconds or in a few seconds while running repeatingly. Through keeping the characteristic impedance, a testing field with extraordinary quality will be produced.

> The testing chamber with large dimensions results from the parallel mounting of the module shown in figure 1 with further modules equal in construction. A change of the field polarization can be reached by turning the arrangement around the length axle of equipment under test.



Impulse production

At first, the IGW is unloaded. Over a triggered spark gap the IGW or all parallel switched IGWs will be charged simultaneously through a high voltage source to a voltage U_o (preferably DC-voltage). The spark gap extinguishes due to the resulting potential equality and the regress of current intensity resulting from this. The impulse will be released independently after approx. 100 ms by closing the rail gap by means of many little arcing channels which connect the IGW with the ICW as a load. With the help of the rail shaped spark gap arises an equal electromagnetic impact of the ICW with the impulse. The maximal width of the rail shaped spark gap and, by this, the width of a module results from manufacturing possibilities.

With the usual excitation of a wave guide at a point, this leads, through the different conductor length, to a time delay of the current on the single wave guides. This delay in time of the wave on the different rods leads, as the inductivity of the spark gap and the change of the characteristic impedance to a obliteration of the flanks of the rectangular shaped impulse and, by this, to a loss in frequency range width of the produced frequency spectrum.

In the case of the rail shaped spark gap the load will be adapted to the impedance of the loading device. Thereby, the initial value of the voltage amounts exactly $U_o/2$. Through the voltage step from U_o to $U_o/2$, a travelling wave will be produced which runs in the directions of the IGW-beginning. After a transmission time τ of the used wave guide the travelling wave reaches the IGW-beginning, will be reflected almost completely at the high resistant spark gap $(r_u=1)$ and a resulting voltage zero arises. After the double running time 2 τ the wave reaches the IGW-end again. With an arcing spark gap, it is completed reflection free $(r_u=0)$. A voltage impulse arises on the ICW. This impulse will jump at the time of switching from zero to $U_o/2$ and after 2 τ again to zero.

Field quality

The whole testing chamber fulfils the sense of the requirements of the ENV 50140 and is suitable for testing the **susceptibility** test relative to the field homogeneity. A comparison extending the requirements of the ENV 50140 onto the three levels in the testing chamber shows



the in fig. 5 illustrated variation between point 14 as reference point and respectively all other measuring points (6 to 12 possible points exceed the 6-dB-criterion).

Patent claims

- 1. Device for testing the electromagnetic compatibility and (EMC)-susceptibility, especially for systems having comparatively large dimensions as wagons and/or trains, with impulse generating wave guides (IGW) which are arranged parallel and show electrical conducting single rods (2) switched together over an head electrode (5), which are connectable over a rail-shaped spark gap (4) in direct line with impulse-conducting wave guides (ICW), which, in return, are connected preferable right angled with an terminating characteristic impedance (6) in order to build up a testing chamber for the system to be tested, which, preferably right-angled attached, with one or several return conductors is switched together, at which the magnitude of the terminating characteristic impedance (6) with, at the most a few ohm difference, correspond to the impulse generating wave guide (IGW).
- 2. Device after claim 1, is characterized that the terminating characteristic impedance (6) which is developed planar or is consisting of several single characteristic impedance's.
- 3. Device after claim 1 or 2, is characterized that several of the devices are switched together as modules in order to lengthen the testing chamber.
- 4. Device after claims 1-3, is characterized that the rail-shaped spark gap (4) is assigned for a tube with variable pressure.
- 5. Device after claims 1-4, is characterized that testing of the systems is practicable repeatingly in the range of nano seconds to seconds.
- 6. Device after claim 1, is characterized that the impulse generating wave guide (IGW) is arranged parallel to the return conductors with essentially the same characteristic wave impedance as the ICW.

Summary

EMV-testing device for systems having large dimensions

According to the law for electromagnetic compatibility of 1 January 1995 all electrical apparatus must have a certain resistance to interference by electromagnetic fields. Especially in the case of systems having large dimensions, such as trains, it is at present not possible to carry out such a test economically using conventional methods. The invention relates to a test device, which makes such a testing possible and beneficial. According to the invention, a test device consists of a novel arrangement of an impulse-generating wave guide (IGW), which consists of parallel, electrically conductive individual rods, which are connected over by a head electrode and, via a rail-like spark gap which is in a straight line with an impulse--conducting wave-guide (ICW) which is identical in structure but longer, is closed at right angles with a terminating resistor. A return line is connected to said terminating resistor. Several of these IGW, ICW, return lines and termination resistors arranged as described above can be connected in parallel in a modular manner via a shared release mechanism and therefore create a testing space suitable for a large system.

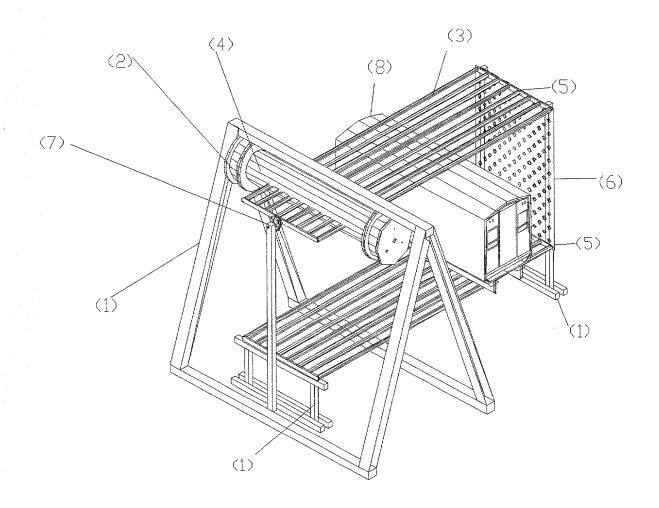


Fig. 1 A performance example of a module with a carrying rack, a high voltage connection and an equipment under test section in vertical polarization

- (1) Rack out of electrical, non-conducting material
- (2) IGW
- (3) ICW
- (4) Pressure tube and rail-shaped spark gap
- (5) Bus bar
- (6) Terminating impedance
- (7) Triggered first spark gap and high voltage source connection

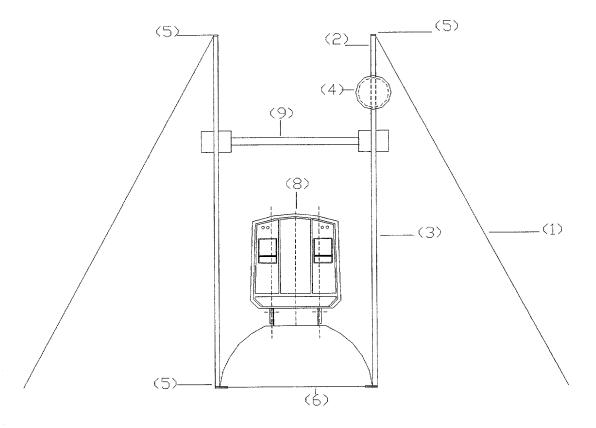


Fig. 2 A performance example of the horizontal polarization

- (1) Wooden rack
- (2) IGW
- (3) ICW
- (4) Pressure tube and rail-shaped spark gap
- (5) Bus bar
- (6) Terminating characteristic impedance
- (7) Triggered first spark gap and high voltage source connection
- (8) Train section in the testing chamber
- (9) Synthetic column

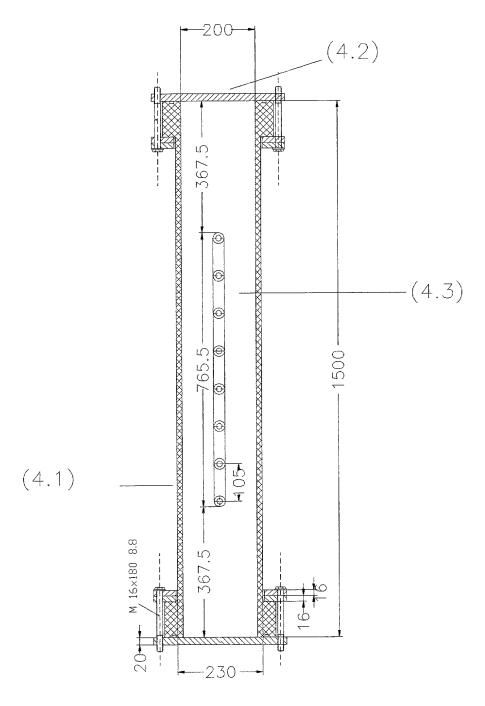


Fig. 3 A performance example of the pressure tube with electrode as detail of figure 1 and figure 2

- (4.1) GFK-tube
- (4.2) Lit
- (4.3) Rail-shaped electrode, serves as connection for the single wave guides at the same time

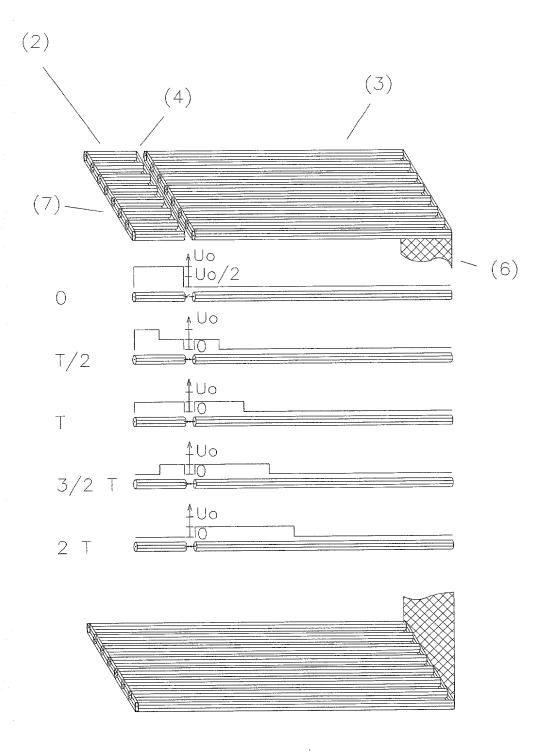


Fig. 4 Function

- (1) IGW
- (2) ICW
- (3) Rail-shaped spark gap
- (4) Terminating impedance

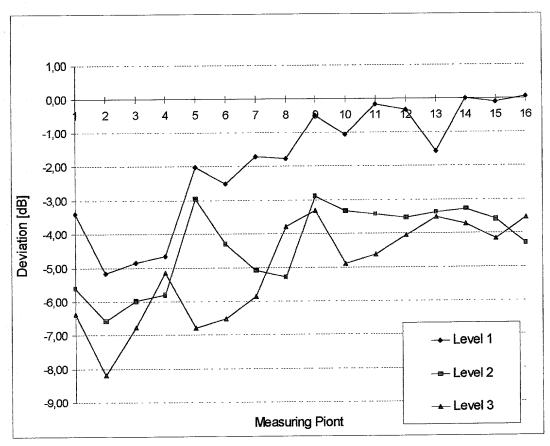


Fig. 5 6-dB-criteria of all measuring points in the testing chamber

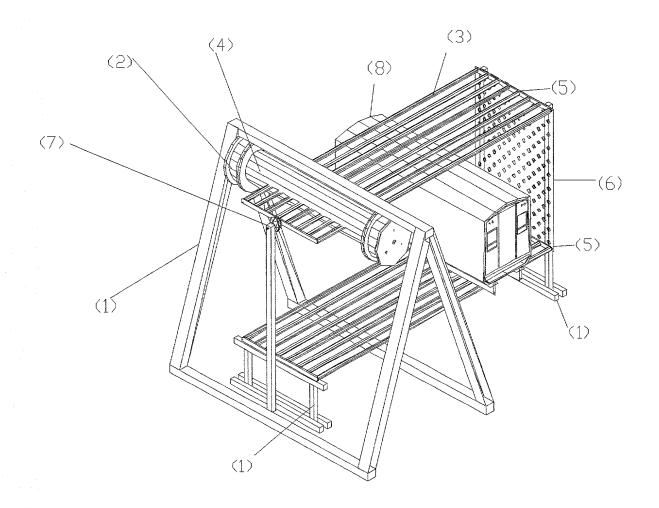


Fig. 1 A performance example of a module with a carrying rack, a high voltage connection and an equipment under test section in vertical polarization

- (1) Rack out of electrical, non-conducting material
- (2) IGW
- (3) ICW
- (4) Pressure tube and rail-shaped spark gap
- (5) Bus bar
- (6) Terminating impedance
- (7) Triggered first spark gap and high voltage source connection

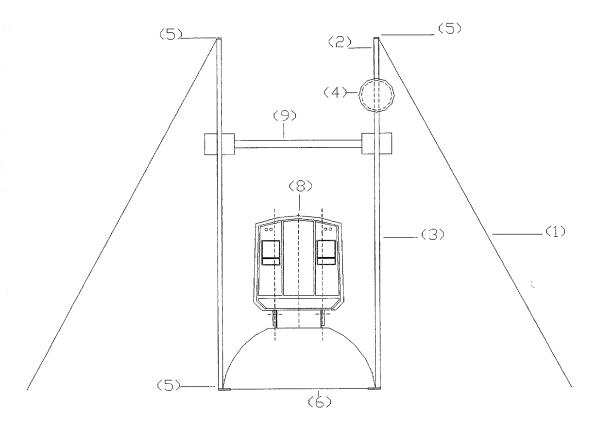


Fig. 2 A performance example of the horizontal polarization

(1) Wooden rack

- (2) IGW
- (3) ICW
- (4) Pressure tube and rail-shaped spark gap
- (5) Bus bar
- (6) Terminating characteristic impedance
- (7) Triggered first spark gap and high voltage source connection
- (8) Train section in the testing chamber
- (9) Synthetic column

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Fig. 3 A performance example of the pressure tube with electrode as detail of figure 1 and figure 2

(4.1) GFK-tube

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- (4.2) Lit
- (4.3) Rail-shaped electrode, serves as connection for the single wave guides at the same time

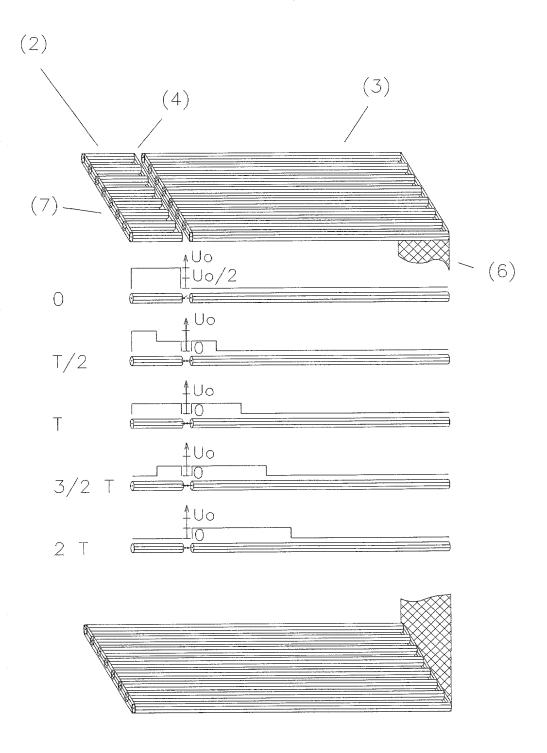


Fig. 4 Function

- (2) IGW
- (3) ICW
- (4) Rail-shaped spark gap
- (6) Terminating impedance

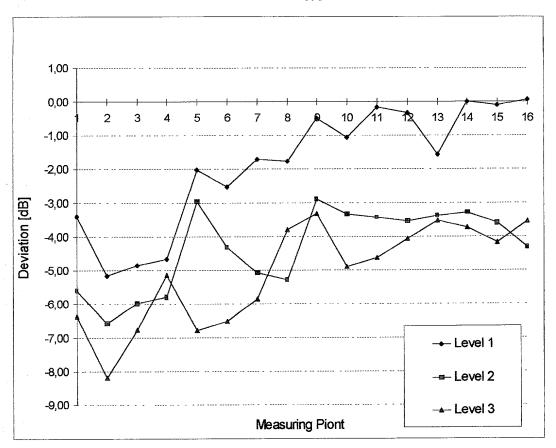


Fig. 5 6-dB-criteria of all measuring points in the testing chamber

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